

MASV method and energy optimization of control parameters

TEXT: RNDr. Milan Konečný, Kabinet matematického modelování, Lašská univerzita libovolného věku

The paper is focused to problems with finite and infinite models, time optimization, energy optimization parameters in the MASV method, called Method Aggregate State Variables.

The MASV method, called Method Aggregate State Variables, and its applications consist of four steps:

- mathematical model,
- control algorithm,
- simulation control,
- application in industry.

Classical formulation of the MASV method does not solve the control in the finite time and construction algorithm uses the control in the infinite time. Time optimization cannot use this formulation. In the paper we show one way of optimization control parameters \mathbf{T}, \mathbf{D} .

Mathematical method of control system

The following mathematical model of the nominal nonlinear subsystem will be considered

$$\dot{\mathbf{x}} = \mathbf{f}(\mathbf{x}, t) + \mathbf{G}(\mathbf{x}, t)\mathbf{u}, \quad \mathbf{x}(0) = \mathbf{x}_0, \quad (1)$$

where

$\mathbf{x} = [x_1, x_2, \dots, x_n]^T$, $\dim \mathbf{x} = n$ is the vector function of state variables,

$\mathbf{u} = [u_1, u_2, \dots, u_m]^T$, $\dim \mathbf{u} = m$

is the vector function of control variables,

$$\mathbf{f} = [f_1, f_2, \dots, f_n]^T, \quad \dim \mathbf{f} = n$$

$\dim \mathbf{f} = n$

is a continuous vector function,

\mathbf{G} , $\dim \mathbf{G} = (n, m)$ is the matrix of

continuous functions $g_{ij}(\mathbf{x})$,

n – number of state variables (the order of the nonlinear subsystem),

n_j – partial order, m – the number of the control variables.

The matrix \mathbf{G} is of the following form

$$\mathbf{G} = \begin{bmatrix} 0 & 0 & \dots & 0 \\ \dots & \dots & \dots & \dots \\ g_{r_1 1} & g_{r_1 2} & \dots & g_{r_1 m} \\ 0 & 0 & \dots & 0 \\ \dots & \dots & \dots & \dots \\ g_{r_2 1} & g_{r_2 2} & \dots & g_{r_2 m} \\ 0 & 0 & \dots & 0 \\ \dots & \dots & \dots & \dots \\ g_{n 1} & g_{n 2} & \dots & g_{n m} \end{bmatrix}$$

$$r_0 = 0; \quad r_j = r_{j-1} + n_j, \quad j = 1, 2, \dots, m,$$

$$n = r_m = \sum_{j=1}^m n_j$$

The condition of controllability of the nominal nonlinear subsystem (1) [Zitek & Viteček 1999]

$$\text{rank } \mathbf{G}(\mathbf{x}, t) = m \quad (3)$$

is assumed.

It is supposed that $i = 1, 2, \dots, n; j = 1, 2, \dots, m$ and strictly not distinguished between a subsystem (system) and a model in the entire the following text.

Control algorithms design – MASV Method

The task of the optimal tracking control design is determination of the feedback control

$$\mathbf{u} = \mathbf{u}(\mathbf{x}, \mathbf{x}^w, t) \quad (5)$$

for the controllable nominal standard nonlinear subsystem (1), which for a given state trajectory $\mathbf{x}^w(t)$ ensures its tracking by a real state trajectory $\mathbf{x}(t)$ so that value of the quadratic objective functional

$$J = \int_0^{\infty} (\mathbf{e}^T \mathbf{D}^T \mathbf{D} \mathbf{e} + \dot{\mathbf{e}}^T \mathbf{D}^T \mathbf{T}^2 \mathbf{D} \dot{\mathbf{e}}) dt \quad (6)$$

$$\mathbf{e} = \mathbf{x}^w - \mathbf{x}, \quad \dim \mathbf{e} = n,$$

$$\lim_{t \rightarrow \infty} \mathbf{e}(t) = \lim_{t \rightarrow \infty} \dot{\mathbf{e}}(t) = 0 \quad (7)$$

is minimal, where \mathbf{e} is the error vector,

\mathbf{D} – the constant nonnegative aggregation matrix [$\dim \mathbf{D} = (m, n)$, $\text{rank}(\mathbf{D}\mathbf{G}) = m$],

\mathbf{T} – the diagonal matrix of positive time constants T_j of the order m , i.e.

$$\mathbf{T} = \text{diag}[T_1, T_2, \dots, T_m] \quad (8)$$

By the method of the aggregation of the state variables, it is possible to obtain the optimal feedback control [Zitek & Viteček 1999]

$$\mathbf{u} = [\mathbf{D}\mathbf{G}(\mathbf{x}, t)]^{-1} \{ \mathbf{T}^{-1} \mathbf{D} \mathbf{e} + \mathbf{D} [\dot{\mathbf{x}}^w - \mathbf{f}(\mathbf{x}, t)] \} \quad (9)$$

which causes the aggregated optimal closed-loop control system

$$\mathbf{D} \dot{\mathbf{e}} + \mathbf{T}^{-1} \mathbf{D} \mathbf{e} = 0, \quad \mathbf{e}(0) = \mathbf{e}_0 \quad (10)$$

and minimal value of the quadratic objective functional (6)

$$J^* = \mathbf{e}_0^T \mathbf{D}^T \mathbf{T} \mathbf{D} \mathbf{e}_0 \quad (11)$$

If the elements d_{jj} of the aggregation matrix \mathbf{D} will be chosen in accordance with the formulas



$$\left. \begin{aligned} d_{ji} &= 0 && \text{for } i \leq r_{j-1} && \text{or } i > r_j \\ d_{ji} &> 0 && \text{for } r_{j-1} < i \leq r_j \\ d_{jj} &= 1 \end{aligned} \right\} \quad (12)$$

then the characteristic polynomial of the aggregated optimal closed-loop control system (10) can be written in the form

$$N(s) = \prod_{j=1}^m N_j(s),$$

$$N_j(s) = \left(\frac{1}{T_j} + s \right) \sum_{p=r_{j-1}+1}^{r_j} d_{jp} s^{p-r_{j-1}-1} \quad (13)$$

where

s is the complex variable in the Laplace transform,

N_j - the characteristic polynomial of the j -th autonomous control subsystem of the partial order n_j .

It is obvious that in this case the optimal closed-loop control system consists of m autonomous linear control subsystems whose desired dynamic behavior can be ensured by a suitable choice of the time constants T_j and coefficients d_{ji} of their characteristic polynomials (13), i.e. by a suitable choice of the matrix \mathbf{T} and \mathbf{D} . It is very important that the quadratic objective functional (6) has only an auxiliary purpose. The feedback control (9) demands knowledge of the exact mathematical model of the nominal nonlinear dynamic subsystem (1). The control \mathbf{u} is non-robust and is often called the equivalent control. It ensures the aggregated optimal closed-loop control system (10) from which after completion with equations

$$\dot{e}_i = e_{i+1}, \quad i \neq r_j \quad (14)$$

the full optimal closed-loop control system can be obtained in the form with a matrix \mathbf{A}

$$\dot{\mathbf{e}} = \mathbf{A}\mathbf{e}, \quad (15)$$

which has the characteristic polynomial (13).

Formulation of some open question in the MASP method

The MASV method was formulated considering

- infinite final time
- constant value of parameters \mathbf{D}, \mathbf{T}
- used method of energy optimization.
- These properties are basic for development of the MASV method.

We will make some remarks to

- finite and infinite models,
- control in the finite time,
- control with error in the finite time,
- optimal control in the time,
- energy optimization of control parameters.

Models with finite and infinite final time and with error in final time

We will rate models according the final time and the error in final time.

Model MASV ($\infty, \mathbf{0}$) – the classical MASV method.

$$J = \int_0^{\infty} \left(\mathbf{e}^T \mathbf{D}^T \mathbf{D} \mathbf{e} + \dot{\mathbf{e}}^T \mathbf{D}^T \mathbf{T}^2 \mathbf{D} \dot{\mathbf{e}} \right) dt \quad (16)$$

$$\lim_{t \rightarrow \infty} \mathbf{e}(t) = \lim_{t \rightarrow \infty} \dot{\mathbf{e}}(t) = \mathbf{0} \quad (17)$$

The final time is infinite and the error in infinity equals to $\mathbf{0}$.

The infinite final time is not realistic.

Model MASV ($t_f, \mathbf{0}$) – basic version with infinite final time and zero error

$$J = \int_0^{t_f} \left(\mathbf{e}^T \mathbf{D}^T \mathbf{D} \mathbf{e} + \dot{\mathbf{e}}^T \mathbf{D}^T \mathbf{T}^2 \mathbf{D} \dot{\mathbf{e}} \right) dt \quad (18)$$

$$\mathbf{e}(t_f) = \dot{\mathbf{e}}(t_f) = \mathbf{0} \quad (19)$$

This model is realistic, but is not usually solvable.

Model MASV (t_f, \mathbf{error}) - version with the finite final time t_f and limited value of $\mathbf{e}(t_f), \dot{\mathbf{e}}(t_f)$

$$J = \int_0^{t_f} \left(\mathbf{e}^T \mathbf{D}^T \mathbf{D} \mathbf{e} + \dot{\mathbf{e}}^T \mathbf{D}^T \mathbf{T}^2 \mathbf{D} \dot{\mathbf{e}} \right) dt \quad (20)$$

$$\|\mathbf{e}(t_f)\|_0 \leq error_0, \|\dot{\mathbf{e}}(t_f)\|_1 \leq error_1 \quad (21)$$

In this model the final time t_f is finite and the error \mathbf{e} is less that constants **error**.

Design control algorithm MASV

(t_f, \mathbf{error})

The aim is to find t_f such that the error \mathbf{e} in the final time is less than **error**. One type of solution is the following algorithm. The main idea is to transform the problem by the method MASV.

Control algorithm:

- find control by using method MASP,
- compile the system of differential equations for errors,
- compute a priori estimate for the solution,
- from a priori estimate calculate the value of t_f

Time eps – optimization using the method MASV (t_f, \mathbf{error})

Formulation of the problem – Find the minimal time t_f , which meets the MASV Model (t_f, \mathbf{eps})

Remarks to the solution of the problem. Design control algorithm MASV (t_f, \mathbf{error}), choose a priori estimate for solution of this problem.

One of the possible ways how to solve this problem is optimizing variables using a priori estimate. We find approximation of solution.

Energy optimization of \mathbf{T}, \mathbf{D}

One of the possible ways how to optimize \mathbf{T}, \mathbf{D} is minimizing the functional

$$J^* = \mathbf{e}_0^T \mathbf{D}^T \mathbf{T} \mathbf{D} \mathbf{e}_0 \quad (22)$$

Minimizing algorithm:

Find the boundaries for parameters \mathbf{D}, \mathbf{T} .

Use Method Lagrange Multipliers.

The paper describes a concept for using the MASV method in the non-standard condition models and algorithms, where the final time is finite and optimization, energy optimization parameters of \mathbf{T}, \mathbf{D} have to be taken into account. Basic algorithms are formulated.



These ideas will be developed and employed on realistic problems in the next author's paper.

Remark: I would like to find co-workers for these problems and we should make a request for a grant.

References

1. KHALIL, H.K. 1996. *Nonlinear Systems*. Second Ed. Upper Saddle River: Prentice-Hall, 1996.
2. ZÍTEK, P. & VÍTEČEK, A. 1999. *Control Design of Anisochronic and Nonlinear Subsystems (in Czech)*. Prague: CTU in Prague, 1999
3. KONEČNÝ, Milan: "MASV metod and controlling in finite time", Transactions of the VŠB – Technical University of Ostrava, Mechanical Series, No. 1, 2009, vol. LIV

4. KONEČNÝ, Milan: "SOME REMARKS TO CONTROL BY MASV METHOD", ICCO 2009, Zakopane, Polsko
5. VÍTEČEK, A. 1990. Algoritmy řízení robotů, Výzkumná práce úkolu SPZV III-8-2/06/05-3, FSE VŠB v Ostravě
6. VÍTEČEK, A. 1992. Optimalizace systémů, *Dynamická optimalizace*, Skripta FS VŠB v Ostravě
7. VÍTEČKOVÁ, M. 1998. *Seřízení regulátorů metodou inverze dynamiky*, Skriptum VŠB-TU Ostrava, ISBN 80-7078-628-0
8. VÍTEČKOVÁ, M. 1998. *Matematické metody v řízení, L a Z transformace*, Skriptum VŠB-TU Ostrava, ISBN 80-7078-570-5
9. VÍTEČEK, A., VÍTEČKOVÁ, M. 1999. *Optimální systémy řízení*. Ostrava, VŠB – TU Ostrava, ISBN 80-7078-736-8
10. VÍTEČEK, A. 2000. *Robust Control for Nonlinear Dynamic Subsystems*, In:

Sborník vědeckých prací VŠB-TU Ostrava, ISBN 1210-0471

11. VÍTEČEK, A. 2002. *Návrh robustního řízení metodou agregace*. Sborník z konference Kybernetika a informatika, Trebišov
12. VÍTEČEK, A. & VÍTEČKOVÁ, M. 2002. *Metoda agregace a robustní algoritmy*, Kouty nad Desnou, Univerzita Pardubice, ISBN 80-7349-452

The paper is focused to problems with finite and infinite models, time optimization, energy optimization parameters in the MASV method, called Method Aggregate State Variables.

RESUME